



Testing the Reliability of Solder Balls

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More Storage with Less Packaging

Problem

- ❑ Dual in-line packages (DIPs) are packages being used for memory and they are changing to denser packaging
- ❑ Connecting components to printed circuit boards (PCBs) requires the lead of components being embedded into drilled holes in PCBs
- ❑ It is not efficient to drill hundreds of holes through PCBs for denser packages

Solution

- ❑ Using smaller pads with solder paste or solder balls to make connections to the board or PCBs
- ❑ Smaller and thinner packaging size, with more output and input channels from a single die, are in high demand

The Experiment



Materials

Solder Balls and Chips Machines

- SAC105 NiAu
- SAC305 NiAu
- SA105 OSP
- Nordson Dage 4000 Plus
- Duster
- Dage Shear 187-0307915163
- Hakko 394

*SAC105 contains 98.5% Tin (Sn), 1.0% Silver (Ag), and 0.5% Copper (Cu).
SAC305 contains 96.5% Sn, 3.0% Ag, and 0.5% Cu

Methods

1. Turning the vacuum and Dage machine on
2. Changing the calibrations using the computer to adjust speeds
3. Performing shear tests
4. Collecting data and plotting it on a graph



Fig. 1(a) Hakko 394 is used to pick up the microchip from suction

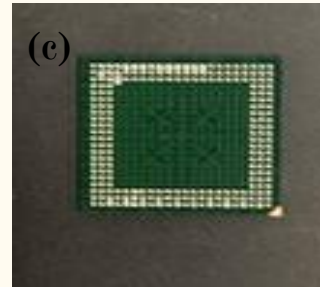


Fig. 1(c) A Ohr SAC105 NiAu chip post shearing



Fig. 1(b) The Nordson Dage 4000 plus is used to perform shear tests

Data



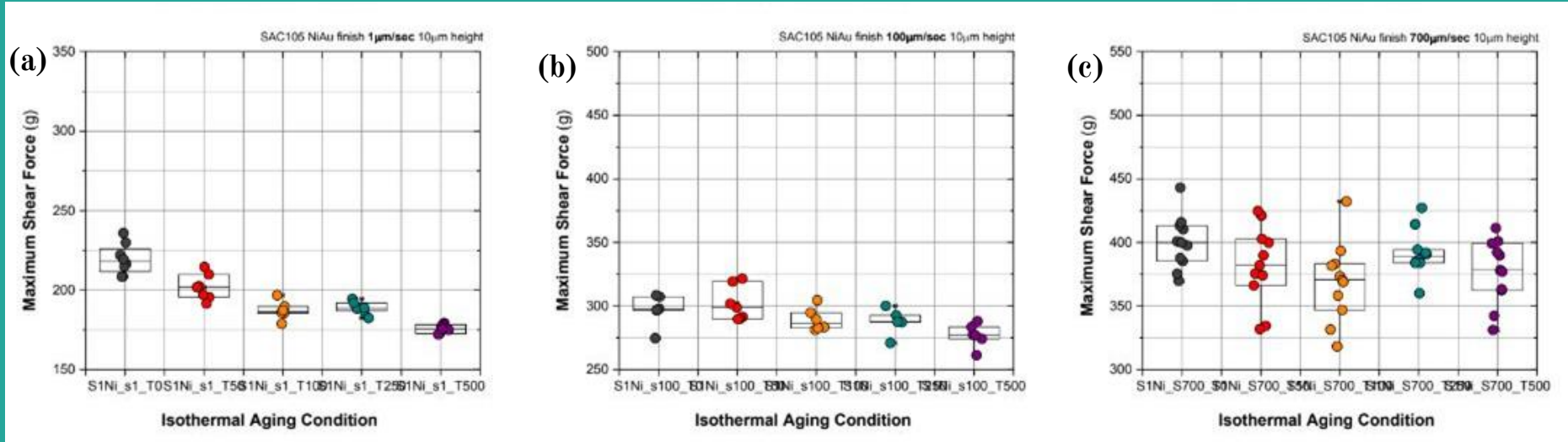


Fig. 2(a) The SAC105 NiAu surface shear test results with 1 μ m/s shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

Fig. 2(b) The SAC105 NiAu surface shear test results with 100 μ m/s shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

Fig. 2(c) The SAC105 NiAu surface shear test results with 700 μ m/s shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

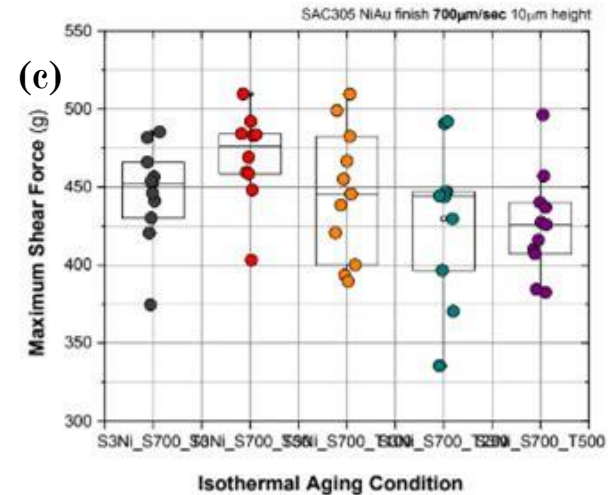
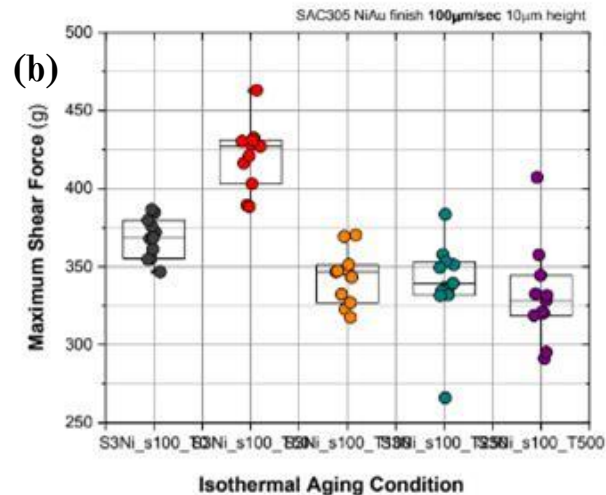
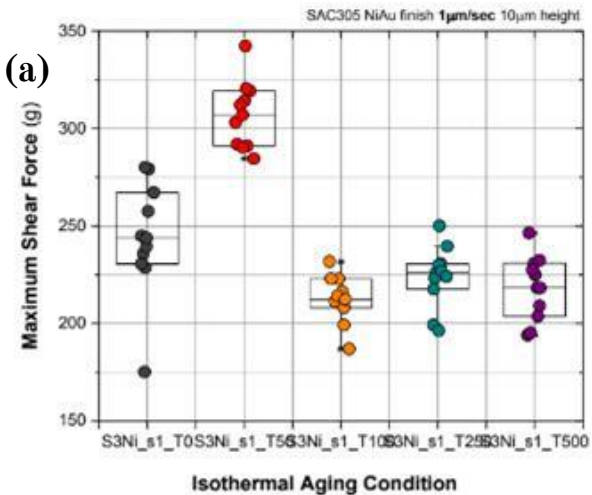


Fig. 3(a) SAC305 NiAu surface shear test results with 1 μ m/sec shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

Fig. 3(b) SAC305 NiAu surface shear test results with 100 μ m/sec shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

Fig. 3(c) SAC305 NiAu surface shear test results with 700 μ m/sec shear speed and 10 μ m shear height at isothermal aging conditions 0hr, 50hr, 100hr, 250hr, and 500hr.

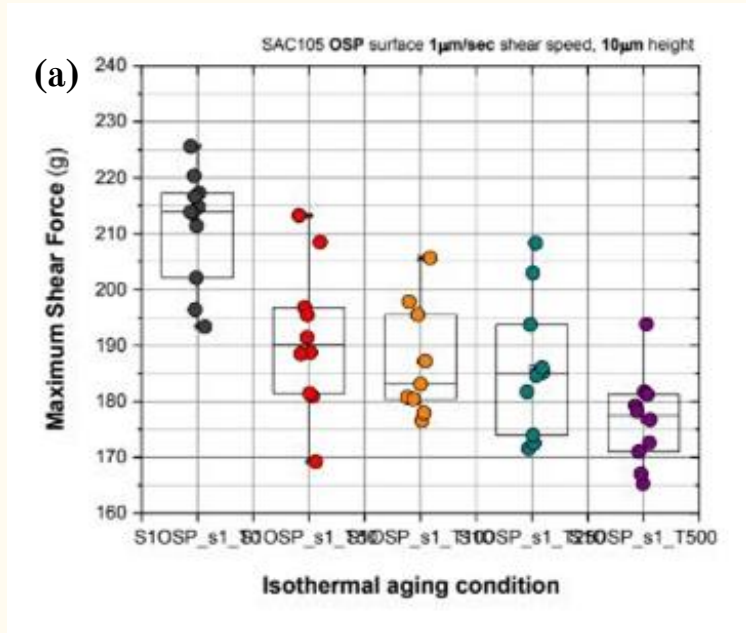


Fig. 4(a) SAC105 OSP surface shear test results with 1µm/s shear speed and 10µm shear height at isothermal aging conditions 0hr, 50hr, 100hr, 100hr, 250hr, and 500hr.

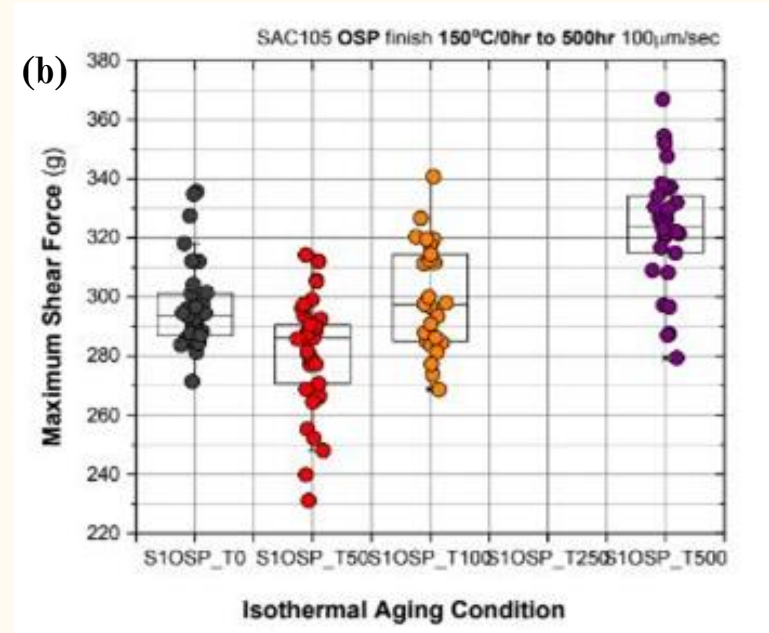


Fig. 4(b) SAC105 OSP 100µm/s shear test results at isothermal aging conditions 0hr, 50hr, 100h and 500hr.

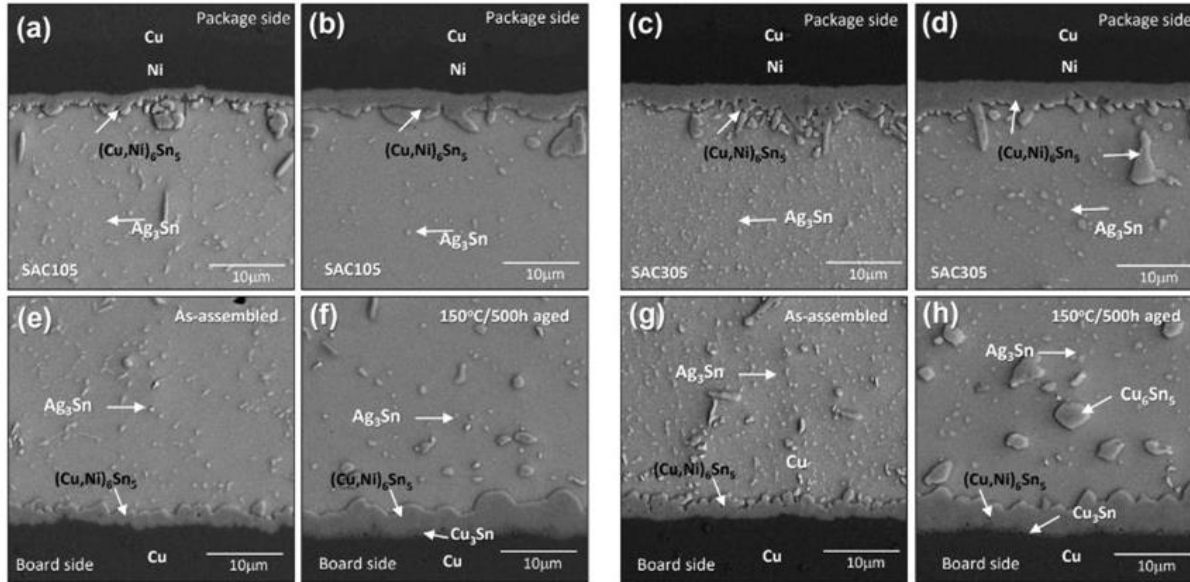


Fig. 5 Scanning electron microscopy cross-section microstructure of SAC105 (a)(e) before aging and (d)(f) after aging at 150°C/500h. SAC305 before aging (c)(g) and after aging at 150°C/500h (d)(h).°C/500h.

Conclusions

- It is recognized that the 700 $\mu\text{m/s}$ test results, in figure 5, do not demonstrate a wide range of distinguishable data. At each aging condition, the average shear forces are close to one another. It would be better to use the 100 $\mu\text{m/s}$ shear test because it gives the best data.
- The average strength of SAC305 NiAu at 500hr aging does not get lower than the average strength of SAC105 NiAu but it does get lower than that of SAC105 OSP.
- The OSP chips have a higher tensile strength, which makes them stronger; however, this means they are also more brittle so if there is a sudden drop they are more likely to break. The SAC105 at a lower age have a lower tensile strength compared to the OSP chips, but they will not break as easily after a sudden drop.



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